

Title : Ethanol Pipeline Optimum Diameter and Cost

		=gpm * 30 minutes		=gpm / 7.481 / 60		
		gallons	gpm	ft ³ /sec	m ³ /sec	
Flow rate qf		90	3	0.006684	0.000189	0.000186 3.290556
Viscosity, cp	1.05	0.0007056 lb/ft-sec		=0.000672	0.00105 pascal-sec	
Density, Sp. Gravity	0.791	49.3584 lb/ft ³		=62.4 * Sp.	790.65 kg/m ³	

low viscosity fluid = assume turbulent; small flow = assume <1" diameter
 assume turbulent <1" diameter = eqn. 9-77 = $0.49 * qf^{0.49} * den^{0.14} * vis^{0.027}$

Diameter Opt.	meters	inches	assume laminar >1" diameter = eqn. 9-78 = $0.863 * qf^{0.36} * vis^{0.18}$		old 4th Edition Eqn's
	0.0115	0.45			inches
	0.0154	0.61	assume turbulent >1" diameter = eqn. 9-76 = $0.363 * qf^{0.45} * den^{0.13} * vis^{0.025}$		0.499 assume laminar >1" diamet
	0.0183	0.72	assume turbulent = eqn. 12-15 = $0.363 * qf^{0.45} * den^{0.13}$	bad eqn in book	0.680 assume turbulent >1" diamet
	0.0155	0.612	inches = $0.49 * (qf^{0.49}) * (den^{0.14}) * (cp^{0.027})$	= $0.49 * (G6^{0.49}) * (G8^{0.14}) * (G7^{0.027})$	0.682 assume turbulent <1" diamet
0.000793	0.0109	0.43	assume laminar <1" diameter = eqn. 9-79 = $1.33 * qf^{0.40} * vis^{0.20}$		0.490 assume laminar <1" diamet

Turbulent Assumption Reynolds Number Check

Diameter Opt.	0.612	inches	~ ID of nominal 1/2" diameter steel pipe, Schd. 40	
Velocity	3.28	ft/sec	= $qf \text{ (ft3/sec)} / (PI()) * ((d/12)^2/4)$	1.00 m/sec
Re = $D V \rho / \mu$	< 2100		= $(d \text{ inch} / 12 \text{ in./ft.}) * (V \text{ ft./sec.}) * (Den. \text{ Lb./ft.}^3) / Vis. \text{ Lb./ft.-sec.}$	
	11,681		greater than 2,100 thus turbulent assumption is valid	Alt.

Actual Inside Diameter	0.824	inches	nominal 3/4" diameter steel pipe, Schd. 40	0.021 meters	0.622 nominal 1/2" diameter steel pipe, Schd. 40
Velocity	1.80	ft/sec	Table 14-2 recommends Velocity between 3 - 10 ft/sec	0.55 m/sec	3.17 Table 14-2 recommends Velocity between 3 - 10 ft/sec
	8,669		much greater than 2,100 thus turbulent assumption is valid		11,485 much greater than 2,100 thus turbulent assumption is v

Schedule Assumption Pressure Rating Check = Ch. 12 Eqn. 14: # = $1,000 * psi / 9000$ or $1,000 * psi / 6500$

Schedule =	16.7	lap-welded 1000/9000 psi			0.493 nominal 3/8" diameter steel pipe, Schd. 40
	23.1	butt-welded 1000/6500 psi	less than 40 thus standard strength Sched. 40 is adequate		5.04 Table 14-2 recommends Velocity between 3 - 10 ft/sec
					14,490 much greater than 2,100 thus turbulent assumption is v

	M&S 2002	M&S now		
Fig.12-4 L	1102.5	1393		
0.02m=0.8"	\$ 45.0	\$56.86	= 3 rd Qtr. 2007 cost per meter	\$13.72 per foot
	105 feet	32 meters		
		\$ 1,819.66	= purchased cost for 3/4" pipe	
		\$1,820.0	dollars	

	M&S 2002	M&S now		
Fig.12-4 r	1102.5	1393		
	\$ 10.00	\$12.63	= 3 rd Qtr. 2007 cost per foot	
	32.004 meters	105 feet		
		\$ 1,326.67	= purchased cost for 1/2" pipe	
		\$1,327.0	dollars	

	\$ 9.00	\$11.37	= 3 rd Qtr. 2007 cost per foot
	32.004 meters	105 feet	

	\$ 1,194.00	= purchased cost for 3/8" pipe
	\$1,194.0	dollars

Ch.E. 453 Fall 2005 Exam #3 Problem #2

Solution Master

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11/30/2007

Biodiesel Transesterification Maximization EVOP

	Catalyst %	Excess EtOH	Temperature	Ave. Yield	Yield1	Yield2	Yield3	Yield4	Yield5	
1	1.00	94	100	90.2	88.8	90.3	89.6	92.1		discard lowest Yield = run 1
2	0.90	94	100	91.7	92.2	90.7	89.7	94		best run 2
3	0.95	100	100	90.7	90.9	89.3	93.4	89.3		run 3
4	0.95	97	120	90.9	90.7	90.5	90.9	91.6		run 4

0.87 100 113.3

discard lowest Yield = run 1

double the average of 3 best and subtract worst coordinates

$$=2*((B8+B9+B10)/3)-B7 \quad =2*((D8+D9+D10)/3)-D7$$

$$=2*((C8+C9+C10)/3)-C7$$

$$=2*((0.90+0.95+0.95)/3)-1.0$$

$$=2*((94+100+97)/3)-94$$

$$=2*((100+100+120)/3)-100$$

Student Scores = 24
 correct = 20 9
 other -1 or 2 2 math errors
 other -12 or more 13 did not average replicates, not EVOP
 maximize -5

correct answers correct method:

9 2

Maximum	Median	Average	Std. Dev.	Minimum
20.0	8.5	13.3	6.2	6.0

Ch.E. 453 Fall 2005 Exam #3 Problem #3

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GOLDEN SECTION SEARCH Reflux Ratio to Minimize Present Worth = 0

Proposal C	Discounted C
0 \$ (78)	\$ (78)
1 \$ 210	\$ 60
2 \$ 230	\$ 18

\$0.0025

PW

$$= (-\$78/(1+i)^0 + 210/(1+i)^1 + 230/(1+i)^2)$$

$$= (B8/(1+\$A\$16)^A8 + B9/(1+\$A\$16)^A9 + B10/(1+\$A\$16)^A10)$$

Golden Ratio = 0.381966

Lower Limit	Upper Limit	Length	Dist.	Point	Cost	
0.05	3	2.95	1.1268	lower 1.1767997	\$ 67.01	< HIGH = Discard
						at Lower & Upper LIMITS: P W
						\$ 330.62
						\$ (11.13)
iteration #1				upper 1.8732003	\$ 22.95	
1.1768	3	1.8232003	0.696401	lower 1.87320023	\$ 22.95	< HIGH = Discard
iteration #2				upper 2.30359947	\$ 6.64	
1.8732	3	1.126799774	0.430399	lower 2.30359943	\$ 6.64	< HIGH = Discard
iteration #3				upper 2.5696008	\$ 1.12	
2.303599	3	0.696400572	0.266001	lower 2.56960077	\$ 1.12	\$ 16.45
iteration #4				upper 2.73399866	\$ 5.26	> HIGH = Discard
2.303599	2.733999	0.430399231	0.164398	lower 2.4679973	\$ 1.68	< HIGH = Discard
iteration #5				upper 2.56960079	\$ 1.12	
2.467997	2.733999	0.266001358	0.101603	lower 2.56960078	\$ 1.12	BEST POINT
iteration #6				upper 2.63239518	\$ 2.76	> HIGH = Discard
2.467997	2.632395	0.164397883	0.062794			

Recommended Discounted Cash Flow ROI between

247% 263%

257.0%

BEST POINT

IRR result= 252.809% \$ 0.000000 Very BEST POINT
 Golden Macro Best= 2.5282571 \$ 0.0046